

Permeability of MgCl_2 - Graphite Reactive Compound

Seyyed Ali Hedayat Mofidi and Kent S Udell*

Department of Mechanical Engineering, University of Utah, USA

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Abstract

Mass transfer limitations due to decreasing permeabilities of the absorbing matrix has been observed to decrease the performance of thermochemical energy storage systems. In this study, the permeability of a reactive complex consisting ammoniated magnesium chloride salt and graphite was measured. It was shown that the permeability of the compound depends on the bulk density of the compound, as well as the amount of NH_3 absorbed in the magnesium chloride matrix. Additionally, the permeability of magnesium chloride (MgCl_2) ammoniate reactive compound is compared with the permeability of the manganese chloride (MnCl_2) reactive compound reported by other researchers. The two salts have similar reactions with ammonia gas with similar reaction kinetics. Although the graphite contents of the reactive compounds were different, it is shown that the permeabilities of both compounds are within the same order of magnitude. However, it is shown that upon absorbing ammonia, the permeability decrease in magnesium chloride compound was larger than the decrease of permeability in the manganese chloride compound.

Keywords: Thermal energy storage; Thermochemical; Porosity; Permeability; Ammonia; Magnesium chloride

Nomenclature

p_{eq} = Equilibrium pressure

T_{eq} = Equilibrium temperature

ΔH_r = Enthalpy of reaction

ΔS_r = Entropy of reaction

\bar{R} = Universal gas constant

ρ_b = Bulk density of compounds

X_g = Global reaction progress

Introduction

Thermochemical energy storage is an attractive form of energy storage to be used by renewable energy systems. Solar thermal powerplants and industrial waste heat storage systems can particularly benefit from thermochemical energy storage systems due to their high energy storage density and long storage period without major losses of the stored energy. The reaction of magnesium chloride salt and ammonia is particularly a good candidate for thermochemical energy storage applications. The high enthalpy of reaction, ($\Delta H_r = \frac{55.7 \text{ kJ}}{\text{mol NH}_3}$) high energy storage density ($1.723 \text{ MJ/kg MgCl}_2 \cdot 2\text{NH}_3$ or 3.27 MJ/kg NH_3), fast kinetics, sustainability of material harvesting, and cost are among the reasons for utilizing magnesium chloride and ammonia reaction. Further energy recovery can be used for food processing, heating, cooling, and refrigeration.

In studying the performance of solid-gas reactive compounds, it was shown that the thermal conductivity and permeability of the reactive compound play an important role in controlling and advancement of the reaction [1-7]. Similarly, in the reaction of ammonia with the magnesium chloride, the permeability of the salt matrix can be the determining factor for the reaction being constrained by the diffusion of either heat or gas through the reactive compound. The permeability of a reactive compound consisting 80%wt. $\text{MgCl}_2 \cdot 2\text{NH}_3$ and

*Corresponding author: Kent S Udell,
Department of Mechanical Engineering,
University of Utah, USA

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20%wt. Expandable Graphite (EG) at different densities of the compound was measured at the fully absorbed ($\text{MgCl}_2 \cdot 6\text{NH}_3$) and fully desorbed ($\text{MgCl}_2 \cdot 2\text{NH}_3$) states and is reported here. It is shown that the permeability of the compound drops as the density of the compound increases. Additionally, absorption of ammonia into magnesium chloride diammoniate salt drops the permeability of the compound further.

Experimental Setup and Procedure

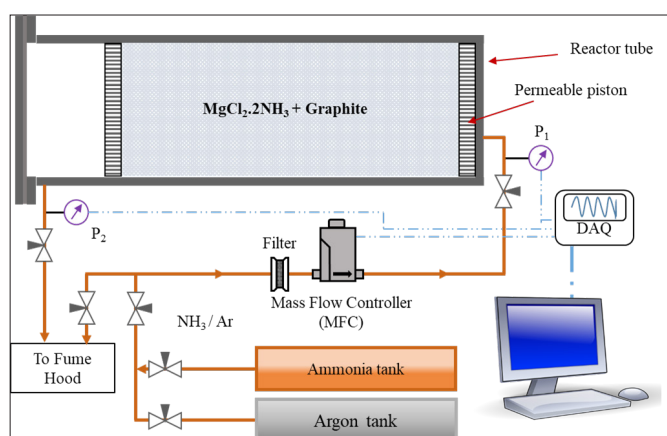


Figure 1: Schematic of the experiment setup.

The permeability of the compound was measured by passing ammonia or argon gas through the reactive compound and measuring the gas flow rate and the pressure difference at both ends of the compound. Figure 1 shows a simplified schematic of the experimental setup. The full description of the setup is given by Hedayat[5]. The experimental setup consists of a tube with an internal diameter of 47.5mm and a length of 250mm made from 316L stainless steel. The tube was filled with salt and graphite complex and two permeable pistons held the complex in place from both ends. During the measurement experiments, the magnesium chloride salt was either in diammoniate (desorbed) or hexammoniate (fully reacted) state to measure the permeability of the compound in the two states of the salt. Since argon gas does not react with the reactive compound, argon was used in measuring the permeability of reactive compound in the desorbed state ($\text{MgCl}_2 \cdot 2\text{NH}_3$). To measure the permeability of reactive compound in fully reacted state ($\text{MgCl}_2 \cdot 6\text{NH}_3$), ammonia gas was used to prevent possible release of ammonia from the compound.

Ammonia and argon gases were supplied from their respective tanks into the supply line which was connected to the Mass Flow Controller (MFC). The MFC controlled and measured the mass flow rate in several steps, going from lower to higher flow rates. In each step, the flow rate was set, and after the flow rate and pressure variations stabilized, the pressures and the flow rate were recorded over one minute. The measurements were averaged for each step

to minimize the measurement errors due to random signal noise.

Two different MFCs were used to measure and control the flow of gas. The first MFC was a P9-B model from MKS Instruments with a full-scale flow rate of 3650 SCCM of NH_3 (5000SCCM of N_2). The accuracy of the MKS mass flow controller was reported as 1% of the set point. Since the flow rate of ammonia from this MFC was not enough for other experiments [8] a second MFC (Hitachi Metals Aera Transformer type FC-PAR7820-C) was used to measure and control the flow rate of the gas into the reactor up to 40000 SCCM of ammonia. The second controller's accuracy was reported by the manufacturer to be 2% of the full-scale range (800SCCM).

Two AST43001F¹ pressure transducers were installed on both ends of the reactor to measure the pressure drop of the gas during the permeability experiments. The accuracy of the pressure transducers has been reported by the manufacturer as $\pm 0.25\%$ of full-scale range, which translates to 8.6kPa. However, the transducers were calibrated by measuring the pressure of saturated ammonia vapor at known temperatures, and the accuracy of the measurement was about 1kPa.

The MKS mass flow controller was directly controlled by a web-app provided by the manufacturer onboard of the unit. The pressure transducers and the Aera Transformer MFC were monitored and controlled by a Jabjack U6 data acquisition (DAQ) module. A Labview program was made for this experimental setup to control the flow rate and read the pressure and flow rate signals.

The raw salt used for all the experiments was 99% pure anhydrous magnesium chloride (MgCl_2) purchased from Alfa Aesar² company, and the graphite was purchased from Asbury Carbons³. The anhydrous magnesium chloride salt was put into the reactor tube and absorbed ammonia gas to form magnesium chloride hexammoniate ($\text{MgCl}_2 \cdot 6\text{NH}_3$). The reacted salt was then heated to 250 °C to release ammonia and form magnesium chloride diammoniate salt ($\text{MgCl}_2 \cdot 2\text{NH}_3$). The pure salt, magnesium chloride diammoniate salt (called desorbed salt), or magnesium chloride hexammoniate salt (called absorbed salt) were mixed with graphite, in a rotating plastic bottle to make a visually homogeneous mixture used for the experiments. The mixture was poured in the reactor using different methods to achieve different compound densities. These methods are fully described by Hedayat[9]. Table 1 lists a description of the six different salt matrices used to measure their permeability in this study.

Density of the compounds (ρ) were measured by measuring the amount of salt and graphite poured into the reactor in each case and measuring the bulk volume of the compound in the reactor. The permeability of the compound was calculated using Equation (1), derived from Darcy's Law and the assumption that the gas behaves as an ideal gas.

¹American Sensor Technologies

²www.Alfa.com

³www.Asbury.com

$$k = \frac{2Q\mu L}{A} \left(\frac{P_{std}}{P_1^2 - P_2^2} \right) \quad (1)$$

In Equation (1), Q is the flow rate measured by the MFC (reported in SCCM), A is the cross section area of the reactor, μ is the dynamic viscosity of the gas, L is the length of the salt compound, P_{std} is the standard pressure (1 atm), and P_1 and P_2 are the pressure at the inlet and outlet of the reactor respectively (as shown in Figure 1).

Results and Discussion

Table 1 lists the measured density and permeability of the reactive compound and Figure 2 shows the permeability of the reactive compound in both absorbed and desorbed states as a function of the density of the desorbed compound ($\text{MgCl}_2 \cdot 2\text{NH}_3$). The uncertainty of measurement for each case is calculated based on Equation (1) and the uncertainty of each measuring instrument. Due to the low uncertainty of the density measurements, the horizontal error bars would be too small to show in Figure 2 and therefore they are omitted.

Table 1: Specification of cases and preparation method for the single-cell reactor experiments.

No.	Case	Description
1	100% MgCl_2 0% graphite 0% compaction	Pure MgCl_2 salt poured into the reactor, and after expansion of salt through absorption of ammonia the volume of the reactor is filled without compressing the salt after.
2	80% $\text{MgCl}_2 \cdot 2\text{NH}_3$ 20% graphite 0% compaction	$\text{MgCl}_2 \cdot 2\text{NH}_3$ salt mixed with 20% wt. graphite, poured into the reactor until it fills the reactor volume.
3	80% $\text{MgCl}_2 \cdot 2\text{NH}_3$ 20% graphite 20% compaction	$\text{MgCl}_2 \cdot 2\text{NH}_3$ salt mixed with 20% wt. graphite poured into the reactor and had pressed to add 20% more mixture than case 2.
4	80% $\text{MgCl}_2 \cdot 2\text{NH}_3$ 20% graphite 40% compaction	MgCl_2 salt mixed with graphite, then mixed with DCM, poured into the reactor until it fills the reactor volume. DCM extracted by evaporation using vacuum and heat. Then the salt is expanded by the absorption of ammonia.
5	80% $\text{MgCl}_2 \cdot 2\text{NH}_3$ 20% graphite 60% compaction	MgCl_2 salt mixed with graphite, then mixed with DCM, poured into the reactor until it fills the reactor volume. DCM extracted by evaporation using vacuum and heat. Then the salt is expanded by the absorption of ammonia.
6	80% $\text{MgCl}_2 \cdot 2\text{NH}_3$ 20% graphite 80% compaction	MgCl_2 salt mixed with graphite, then mixed with DCM, poured into the reactor until it fills the reactor volume. DCM extracted by evaporation using vacuum and heat. Then the salt is expanded by the absorption of ammonia.

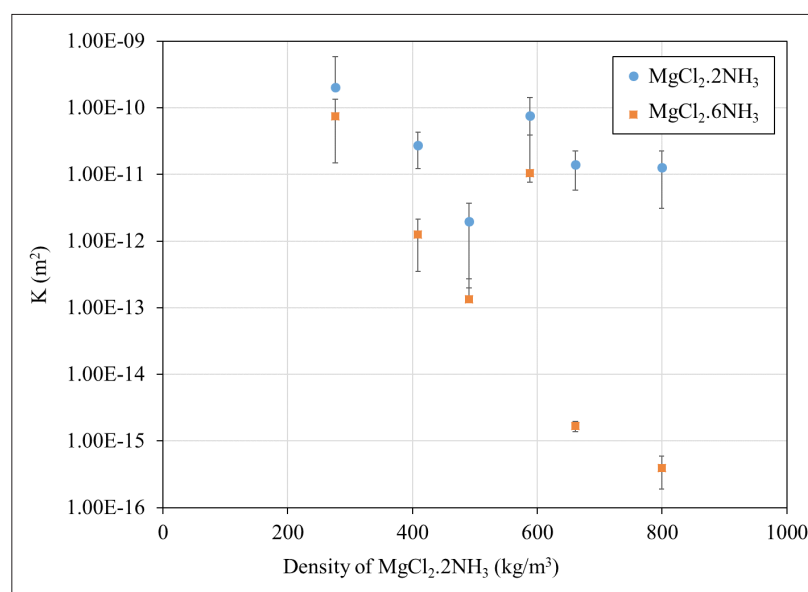


Figure 2: Measured permeability of the reactive compounds.

Figure 2 shows that for each of the cases, the overall permeability of the compound reduces upon absorption of ammonia into the magnesium chloride salt. This is due to the ammonia gas diffusing into the crystalline structure of the desorbed salt [10,11]. Additionally, increasing the density of the compound decreases

its porosity (ϵ), which decreases the overall permeability of the compound as well. As it was shown by [1,3,4] and Hedayat[9] the reduction of the permeability of the compound below 10^{-15}m^2 can have a significant effect on the transport behavior of the ammonia in the reactive compounds (Table 2).

Table 2: Density, porosity, and permeability of the reactive compound for all the cases at both desorbed and saturated states.

Case		$\text{MgCl}_2 \cdot 2\text{NH}_3$			$\text{MgCl}_2 \cdot 6\text{NH}_3$		
No.	Description	$\rho(\text{kg} / \text{m}^3)$	ϵ	$K(\text{m}^2)$	$\rho(\text{kg} / \text{m}^3)$	ϵ	$K(\text{m}^2)$
1	Pure salt, No graphite	276.2	0.84	2.04E-10	421.7	0.66	7.40E-11
2	20% graphite, no compaction.	334.3	0.77	2.74E-11	510.5	0.55	1.25E-12
3	20% graphite, 20% compaction.	417.4	0.71	1.96E-12	637.5	0.44	1.34E-13
4	20% graphite, 40% compaction.	588.2	0.667	7.54E-11	835.2	0.367	1.05E-11
5	20% graphite, 60% compaction.	661	0.604	1.41E-11	938.6	0.246	1.69E-15
6	20% graphite, 80% compaction.	799.4	0.572	1.28E-11	1135.1	0.187	3.91E-16

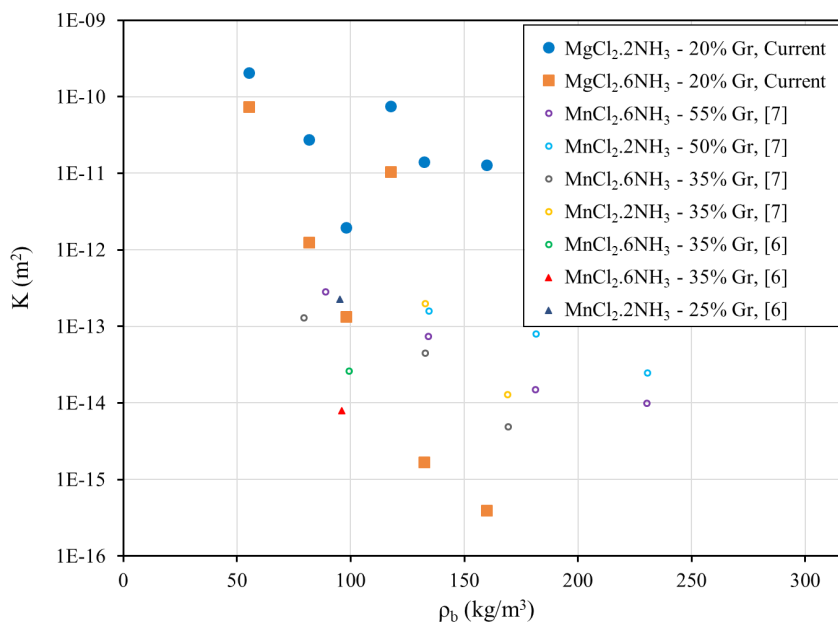


Figure 3: Comparison of permeability measurements with other studies [6,7].

Figure 3 shows a comparison of the measured permeability of magnesium chloride (MgCl_2) and graphite reactive compounds with the values reported by Han [7] & L'Haridon [6] for manganese chloride (MnCl_2) and graphite compounds. Manganese chloride salt reacts with ammonia in a manner similar to magnesium chloride

with similar reaction kinetics and can be used in a thermochemical energy storage system as well. The measurements by Han [7] & L'Haridon [6] were conducted on reactive complexes with more graphite content, and different preparation methods. Comparing the measurements based on the density of the graphite binder shows

the permeability drop for magnesium chloride (MgCl_2) complexes is greater than the permeability drops of manganese chloride (MnCl_2) complex, which could be due to the bigger contribution of the salt grains in the permeability for magnesium chloride reactive compounds in our experiments. It would be beneficial to match the permeability measurements for such compounds with empirical equations for calculation of permeability to determine the importance of salt grain sizes, internal crystalline structure, overall porosity of the compound as it absorbs ammonia.

The large variation in the permeability of the magnesium chloride compound as the reaction goes to completion, coupled with the conclusion that permeability constrains the absorption and heat generation rates [5,8,9], is of concern when a thermochemical energy storage device using this compound is designed. During operation as an absorbent for the NH_3 gas the reaction front travels from the cooled surface much as ice grows from a cold surface. When such mass transfer limitations are present, the permeability of the compound in the cooled region drops orders of magnitude, blocking the flow of the gas and reducing the gas absorption and heat generation rates [5,8,9]. Conversely, when the device is recharged by heating, the desorbed NH_3 vapor will have limited pathways for removal, increasing pressures and equilibrium temperatures, thus reducing heat absorption rates.

Conclusion

The permeabilities of magnesium chloride and graphite compound at six different densities were measured. It was shown that the permeability of the compound decreases with an increase in the bulk density of the compound, or as the compound absorbs ammonia. The measured permeabilities show a similar magnitude and trend with other reported measurements for a similar compound. However, the permeability of magnesium chloride

compounds used in this study show a bigger variation between the desorbed and absorbed states compared to manganese chloride compound with higher graphite content.

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