

# Correlation Between Swelling and Elasticity of Graphene Oxide-Polyacrylamide Composites

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## Abstract

Composites of Graphene Oxide (GO) and Polyacrylamide (PAAm) have been proposed as promising biomaterials for biomedicine and tissue engineering. The aim of this work is to investigate the relationship between swelling and mechanical properties of these composites and demonstrate the role of Graphene Oxide (GO) on the swelling and elasticity of the composites. Swelling experiments were performed in distilled water at 30 °C, monitoring the steady-state fluorescence intensity in real time, using Py in the GO-PAAm composites as a fluorescence probe. The diffusion coefficients,  $D_{sc}$  and the cooperative diffusion coefficients  $D_{em}$  were calculated using Fick's model and Li-Tanaka equations, respectively. The mechanical properties of the composites were investigated by the compression test before and after the swelling process. The GO content dependence of the shear modulus of the composites due to the volume phase transition was measured at 30 °C. After the swelling process, the shear modulus of GO-PAAm composites decreases with the increase of GO content above 8  $\mu$ l GO, indicating a critical value. An increase in GO content leads to a decrease in swelling capacity due to more cross-links and cross-link densities in the composites.

**Keywords:** Graphene oxide; Polyacrylamide; Swelling; Elasticity; Composite

**Abbreviations:** GO: Graphene Oxide; PAAm: Polyacrylamide; SEM: Scanning Electron Microscopy; PVA: Polyvinyl Alcohol

## Introduction

Graphene Oxide (GO) is a lightweight material that has very high strength and thermal stability [1]. It is a two-dimensional carbon material with a thickness of about one atom [2]. Therefore, it is popular material to use in biotechnology, medicine [3] and tissue engineering [4]. In addition, it is an effective filler for improving the electrical, mechanical, and thermal properties of composite materials [2]. The mechanical and thermal properties of Poly (Acrylamide) (PAAm) hydrogels have been modified by the addition of GO [2]. N, N-methylenebisacrylamide (BIS) crosslinks PAAm hydrogels but has several disadvantages such as weakness and brittleness. When GO is added to a hydrogel containing BIS, toughness and tensile strength improve. The content of GO and BIS affects the thermal and mechanical properties of these hydrogels. In addition, GO-BIS gels were observed to have a lower equilibrium swelling ratio than the BIS gels [2]. GO/Polyvinyl Alcohol (PVA) composite film is prepared to observe mechanical strength [5]. When the content of GO is increased, the tensile strength of the composite film initially increases rapidly compared to the pure PVA composite film. The optimum mechanical performance of the film is achieved at a

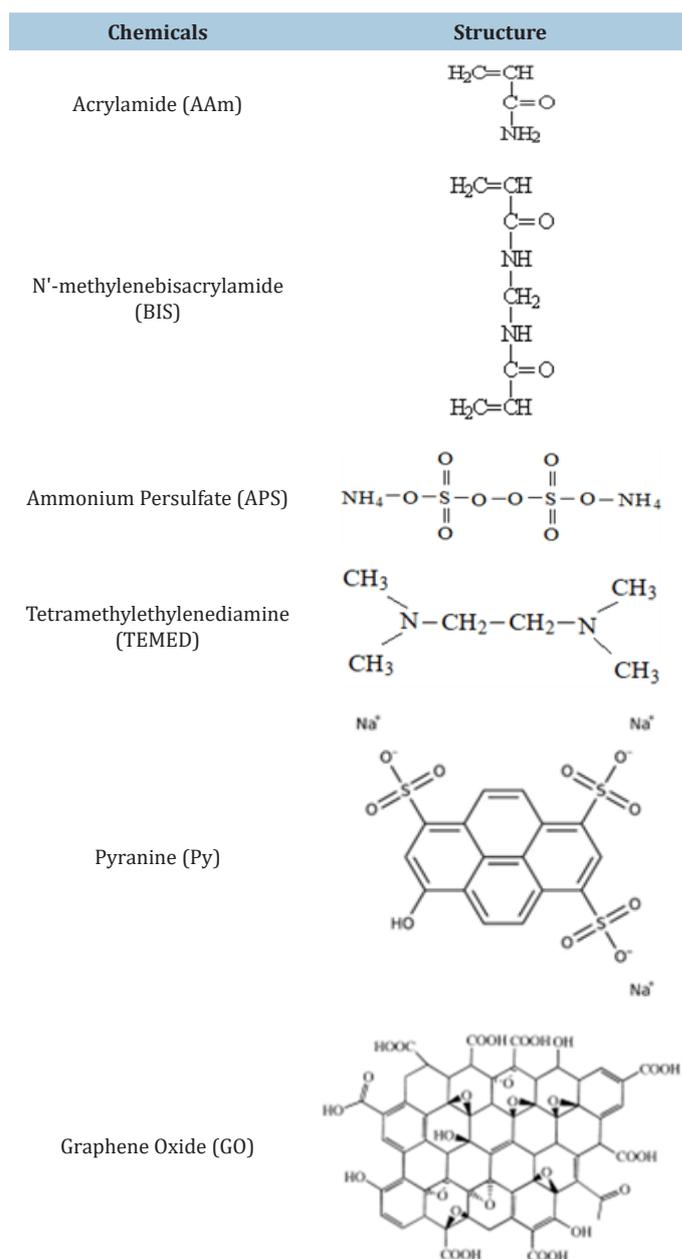
content of 20% of GO by increasing the tensile strength by more than 500% [5]. The pristine GO, silane-functionalized GO (I-GO) and PVI-grafted GO (PVI-g-GO) nanosheets were used to prepare epoxy resin composite to investigate their mechanical and thermal properties [6]. Nanocomposites containing 0.25wt % PVI-g-GO exhibited 59.6% and 45.5% higher tensile strength and modulus, respectively, compared to normal epoxy resin. The result of Scanning Electron Microscopy (SEM) shows a tough structure with a rough surface, which is confirmed by the developed tensile strength [6]. Extrusion-based 3D-printing was used to produce Graphene Oxide (GO)-reinforced HA/gelatin composite scaffold [7]. In this research, mechanical properties of HA/gelatin composite were reinforced by GO. Especially, %15 increase of compressive strength and %22 increase of flexural strength were observed addition to %0.5 GO content. According to these experimental results, GO is potential material to produce composite bone scaffolds and develop mechanical properties for application of bone tissue engineering [7].

In this study, the mechanical and swelling behaviour of GO-PAAm composites and the correlation between these two properties are investigated. The fluorescence method was used to observe the swelling kinetics of GO-PAAm composites. The swelling behaviour of the composites was modelled using Fick's model and the Li-Tanaka equation. On the other hand, the behaviour of the mechanical properties was determined by compressive technique at 30 °C. The composites were examined before and after swelling in water for mechanical measurements. The mechanical behaviour was modelled by the theory of rubber elasticity. It was found that both the swelling behaviour in water and the mechanical properties of the composites were combined for the estimation of physical parameters depending on GO.

## Experiment

### Preparation of composites

GO content (Graphene Oxide, Graphenea) in a concentration 0, 8, 20, 30, 40 and 50 $\mu$ l and 2M AAm (acrylamide, Merck) were used to prepare composites at room temperature. The concentration of GO obtained from Graphenea is 4mg/ml. The purity of GO is over 95% (wt). 1.42g AAm, 0.02g N'-methylenebisacrylamide (BIS, Merck), 0.016g ammonium persulfate (APS, Merck) and 6 $\mu$ l Tetramethylethylenediamine (TEMED, Merck) were dissolved as a homogeneous solution in 10ml distilled water (pH 6.5) at 200rpm for 15min. GO is added to the solution before mixing TEMED. Pyranine (Py) in the GO-PAAm composites was used as a fluorescent probe. Py is a pyrene derivative with three SO<sub>3</sub><sup>-</sup> groups, so Py can be incorporated into the gels by coulombic attractive forces. GO-PAAm composites were prepared by the method of radical crosslinking copolymerization. Immediately before the addition of TEMED, the sample was deoxygenated with bubbling nitrogen for 10 minutes. The solution of 10ml was poured into the injector for swelling and mechanical experiments. The composites were cut from the syringes at room temperature in the form of discs with a diameter of 10mm and a thickness of 4mm [8]. Chemicals are given in Figure 1.



**Figure 1:** The chemical structures of Acrylamide (AAM) as monomer, N'-methylenebisacrylamide (BIS) as crosslinker, Ammonium Persulfate (APS) as initiator, Tetramethylethylenediamine (TEMED) as accelerator, Pyranine (Py) as fluorescence probe as and Graphene Oxide (GO) as nanoparticle, respectively.

### Optical measurements

A spectrometer model LS-55 from Perkin Elmer was used to measure the fluorescence intensity of Pyranine (Py) during the swelling experiments. The spectral band was kept at 5nm while the measurement was performed at 900nm. The disc-shaped composites were in a 1x1x4.5cm<sup>3</sup> square quartz cell with stainless steel wire. The square quartz cell was filled with distilled water to determine the swelling behaviour of the composite. The excitation intensity chosen for the in-situ fluorescence experiments was 340nm. The scattered light intensity,  $I_{sc}$  and emission light intensity

$I_{em}$  of the pyranine was observed as a function of the swelling time at 340nm, and 427nm to show the change in gel structure. Water diffusion is directly proportional to the emission light intensity,  $I_{em}$  and the intensity of the scattered light,  $I_{sc}$  [8]. Thus, when water diffusion increased,  $I_{sc}$  and  $I_{em}$  increased due to the increase in structural heterogeneity of the composite [9].

### Mechanical measurements

An Instron 3340 testing machine with a loading capacity of 500N was used for the pressure measurements. The different amounts of GO doped composites were prepared in an injector with a diameter of 10mm. They were then cut into 4mm thick slices to use two samples each before and after swelling. The diameter of each slice was measured at least three times with a calibrated digital compass (resolution: 0.01mm). Uniaxial compression tests were performed with an Instron 3340 testing machine for different GO contents of the composites. Before swelling, the pressure measurements were taken at a probe size of 10cm, a speed of 0.1mm/min and an over deformation ratio of 40% at 30 °C. Prior to swelling, the pressure expansion (mm) curves and the pressure load F(N) were measured for 0, 8, 20, 30, 40 and 50 $\mu$ l of the composites using GO at 30 °C. The composites were placed in distilled water to achieve swelling equilibrium at 30 °C and to measure compression for the swelling process. The distilled water was changed at least twice. The samples were kept at room temperature for 1 week. This process is called final washing to achieve swelling equilibrium and to remove unreacted repeated units from the composites. Compression measurements after swelling were performed using the same method as described above.

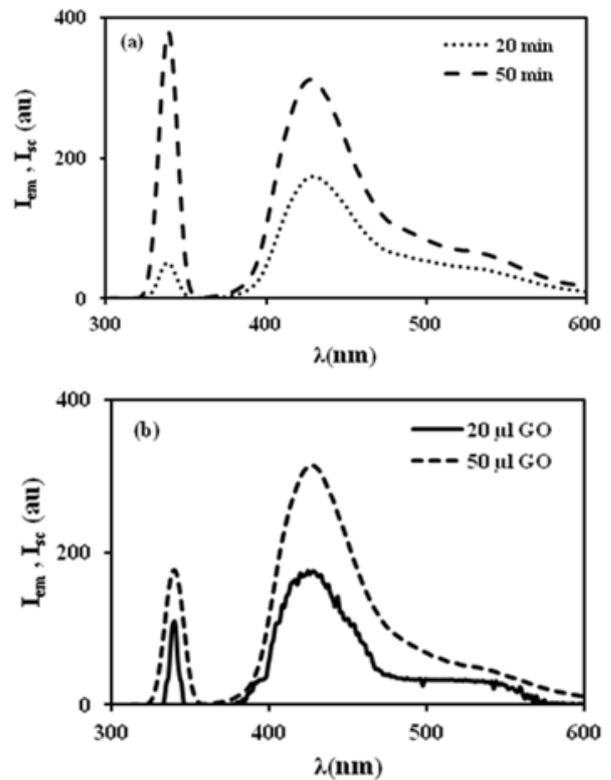
## Results and Discussion

### Diffusion and swelling

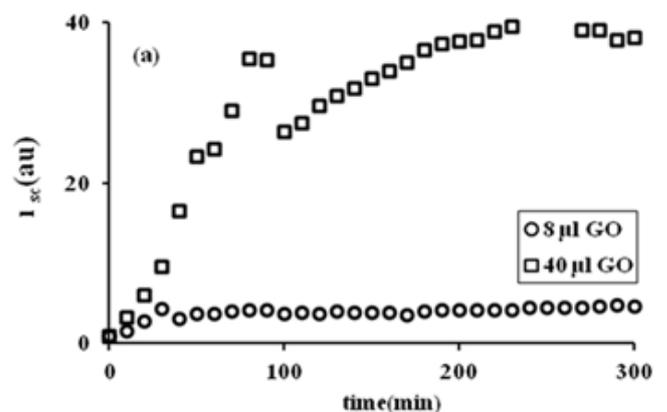
The fluorescence spectra of pyranine in the composites were observed during swelling at 20 and 50 minutes for 50 $\mu$ l content of GO doped composites, as shown in Figure 2a.  $I_{em}$  and  $I_{sc}$  increased when water uptake was increased during swelling. In Figure 1, the fluorescence spectrum of swelling of 20 and 50 $\mu$ l of doped PAAM composite at 100min and 30 °C is shown by different lines. As can be seen in Figure 2b,  $I_{sc}$  and  $I_{em}$  increase with increasing GO content in the distilled water, resulting in high shielding and more lattice heterogeneities [10]. The change in scattered light intensities  $I_{sc}$  as a function of swelling time of the GO-PAAM composites is shown in Figure 3a during the swelling process for 8 and 40 $\mu$ l GO at 30 °C. Assuming that  $I_{sc}$  is proportional to the number of water molecules entering the composite, the behaviour of the intensity curves in Figure 3a suggests that the water molecules are absorbed by the composite network and cause more scattering. This assumption can be explained by "frozen blobs". It is well known that a "frozen blob" appears where two junctions are positioned on adjacent lattice sites [11]. Here we can assume that the penetration of water into the composite is lower in gels with high GO content than in gels with low GO content, which is due to lower solubility and/or high shielding. Based on this picture, the diffusion process can be described using Fick's diffusion model. In this case, the GO-PAAM

composites are considered as thin plates and the solution of the equation is given by the following equation [12].

$$\frac{M}{M_{\infty}} = 1 - \sum_{n=0}^{\infty} \frac{8}{(2n+1)^2 \pi^2} \exp\left(-\frac{D(2n+1)^2 \pi^2 t}{d^2}\right) \quad (1)$$



**Figure 2:** Fluorescence spectra of pyranine in the composites prepared with (a) 50 $\mu$ l of GO during the swelling process at 30 °C for 20 and 50min, and (b) 20 and 50 $\mu$ l of GO at 100min. and 30 °C, respectively.

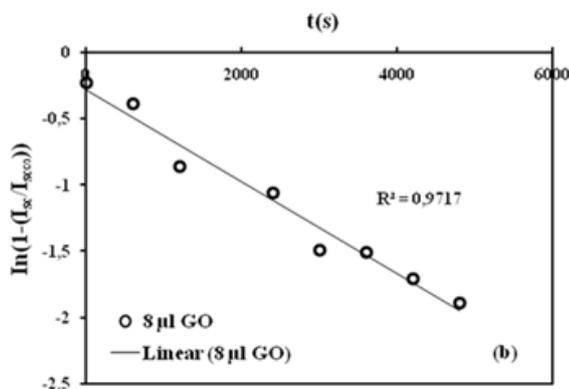


**Figure 3(a):** Scattered light intensities,  $I_{sc}$  versus time,  $t$  during swelling process for 8, and 40 $\mu$ l of GO content

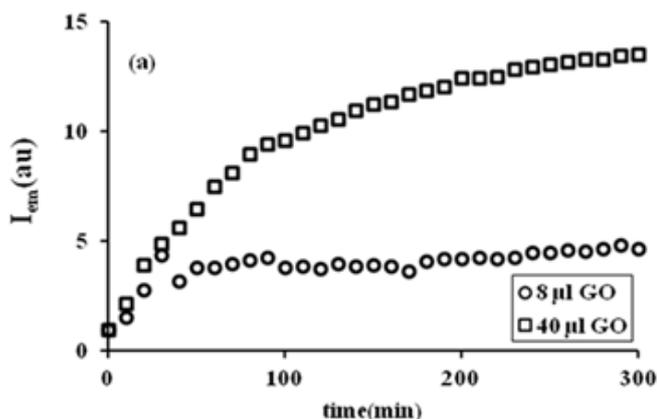
where  $d$  is the thickness of the sample and  $M$  and  $M_{\infty}$  are the masses of water absorbed at time  $t$  and  $\infty$  respectively. Then the logarithmic form of Eq.1 for  $n=0$  can be given as follows:

$$\ln\left(1 - \frac{I_{sc}}{I_{sc\infty}}\right) = \ln \frac{8}{\pi^2} - \frac{D_{sc}\pi^2}{d^2} t \quad (2)$$

where the scattered light intensity  $I_{sc}$  is proportional to the mass of water absorbed at time  $t$ .  $D_{sc}$  is the diffusion coefficient from the scattered light intensity and  $d$  is the thickness. In Fick's diffusion model, the curve in Figure 2a should be linear with respect to Equation 2 and have a slope from which the diffusion coefficient  $D_{sc}$  can be calculated. The curves in the form of equation 2 for 8  $\mu$ l GO in the composites are shown in Figure 3b. It was observed that the slope of the regression lines corresponding to the diffusion coefficient is shown in Figure 4a. Here it can be seen that high  $D_{sc}$  values are observed for composites with low GO content, which is expected due to low shielding and/or high solubility. With increasing GO content, the  $D_{sc}$  values decrease due to the low accessibility of the composite for water molecules.



**Figure 3(b):** logarithmic form of the data in Figure 2(a) by using Eq. 2 for 8  $\mu$ l of GO content at 30 °C, respectively.



**Figure 4(a):** The fluorescence intensities,  $I_{em}$  versus time,  $t$  during swelling process for 8, and 40  $\mu$ l of GO content.

The fluorescence intensity,  $I_{em}$  versus swelling time is shown in Figure 4a for 8 and 40  $\mu$ l of GO doped composites at 30 °C, respectively. It can be seen in Figure 4a that  $I_{em}$  increases with increasing swelling time, indicating that the composite becomes more transparent with increasing water uptake and more Py

molecules leak out, resulting in higher emission. A low  $I_{em}$  intensity at a high GO content indicates that more lattice heterogeneities are present during water uptake of the composite. Therefore, the  $I_{em}$  intensity in the composite is low at a high GO content. During the swelling process, when water molecules enter the gel, more structural complexities are formed, so that  $I_{em}$  in a gel with a high GO content has lower values than in a gel with a low GO content. With this behaviour, equation 3 can be written in terms of  $I_{em}$ . The curves of this typical solvent uptake correspond to the Li-Tanaka equation [8],

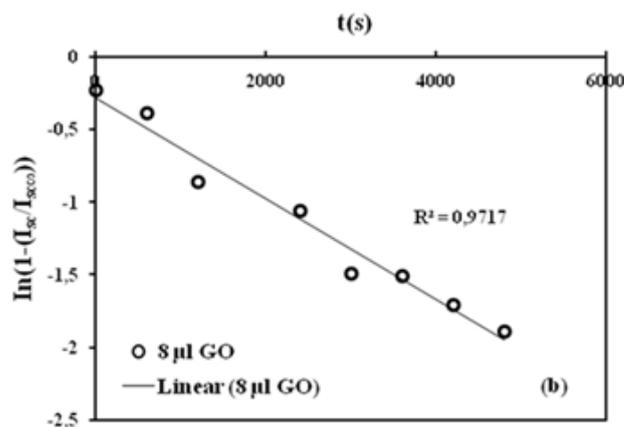
$$\frac{W}{W_f} = 1 - B_1 \exp\left(-\frac{t}{\tau_1}\right) \quad (3)$$

where,  $\tau_1$  is the time constant, measured by the fluorescence technique,  $B_1$  is related to the ratio of the shear modulus,  $\mu$  and longitudinal osmotic modulus,  $M$  and  $t$  is time. The following relationship was derived from Equation 3 to fit the logarithmic form of the data in Figure 4a.

$$\ln\left(1 - \frac{I_{em}}{I_{em\infty}}\right) = \ln B_1 - \frac{t}{\tau_1} \quad (4)$$

Where  $\tau_1$  is the time constant, and values are used to create the linear regression of the curves using equation (4). The linear regression of the curves is shown in Figure 4b. R graph are based on the method described by Li and Tanaka. Considering these graphs, R values were obtained from  $B_1$  and R graph, then  $\alpha_1$  was obtained from  $\alpha_1$  and R graph, respectively. Then the following equation (5)

$$D_{em} = \frac{3\alpha_f^2}{\tau_1\alpha_1^2} \quad (5)$$



**Figure 4(b):** The linear regression of the data in Figure 3(a) fitted to the Li-Tanaka Model (Eq. 4) for 8  $\mu$ l of GO content at 30 °C.

was used to determine the cooperative diffusion coefficients  $D_{em}$  of these disc-shaped composites, and they are about  $10^{-9} \text{m}^2/\text{s}$ , as shown in Figure 4b. It was observed that composites with a high content of GO swell much slower, resulting in smaller  $D_{em}$  coefficients for all measurements at a given temperature. The  $D_{em}$  values decrease with increasing GO content, which is due to the

increasing stiffness of the gel system, i.e., the low accessibility of the composite due to low solubility.

**Elasticity**

From classical thermodynamics the equation of state for rubber elasticity may be expressed as [13],

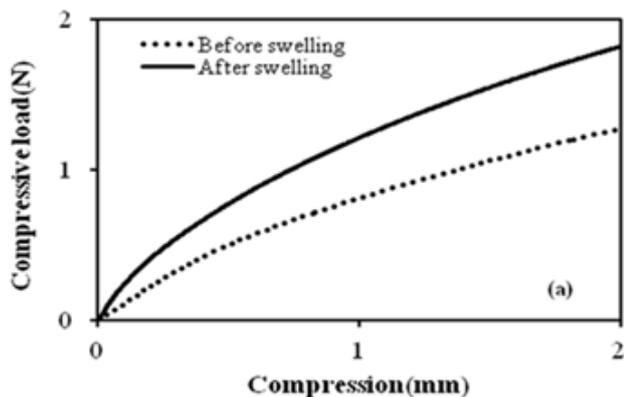
$$f = -k \left( \frac{\partial \ln \Omega(r, T)}{\partial r} \right) \quad (6)$$

where,  $k$  is the Boltzmann constant,  $r$  is a certain end-to-end distance, and  $\Omega(r, T)$  is the probability that the polymer chain with an end-to-end distance  $r$  at temperature  $T$  will adopt a certain conformation. After evaluation of eq. (6), the statistical thermodynamic equation of state for rubber elasticity is obtained below

$$\tau = \left( \frac{\partial A}{\partial \lambda} \right)_{T, V} = \frac{\rho R}{M_c} \frac{r_0^2}{r_f^2} (\lambda) \quad (7)$$

Here,  $\tau$  is the shear stress per unit area,  $\rho$  is the density of the polymer,  $M_c$  is the number average molecular weight between crosslinks, and  $\lambda$  is the extension/compression ratio. Extension/compression ratio,  $\lambda$  changes by different theories [13]. The quantity  $\frac{r_0^2}{r_f^2}$  is the ratio of the end-to-end distance in a real network versus the end-to-end distance of isolated chains. Network imperfections such as cycles, chain entanglements, and chain ends are not considered. The loaded composites were tested for elastic behaviour using uniaxial compression tests for all GO contents at 30 °C. Figure 5a shows the force- compression curves before and after swelling for 40µl of the contents of GO at 30 °C. From the rubber elasticity [14-16] the change in the length of the compressed sample,  $\Delta L$ , is given in equation (8)

$$\Delta L = L_0 - L \quad (8)$$



**Figure 5(a):** Force versus compression.

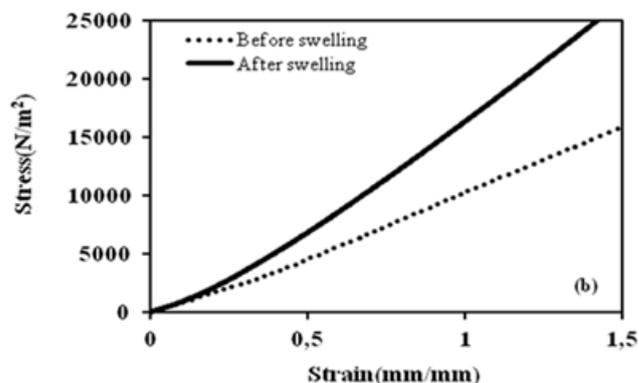
Where is the  $L_0$  original length of the specimen and  $L$  is the deformed length of the specimen along the vertical axis. The compressive stress was calculated according to the following equation (9)

$$\sigma = f/A \quad (9)$$

where  $f$  and  $A$  are the applied force and the initial cross-sectional area of the specimen perpendicular to the direction of

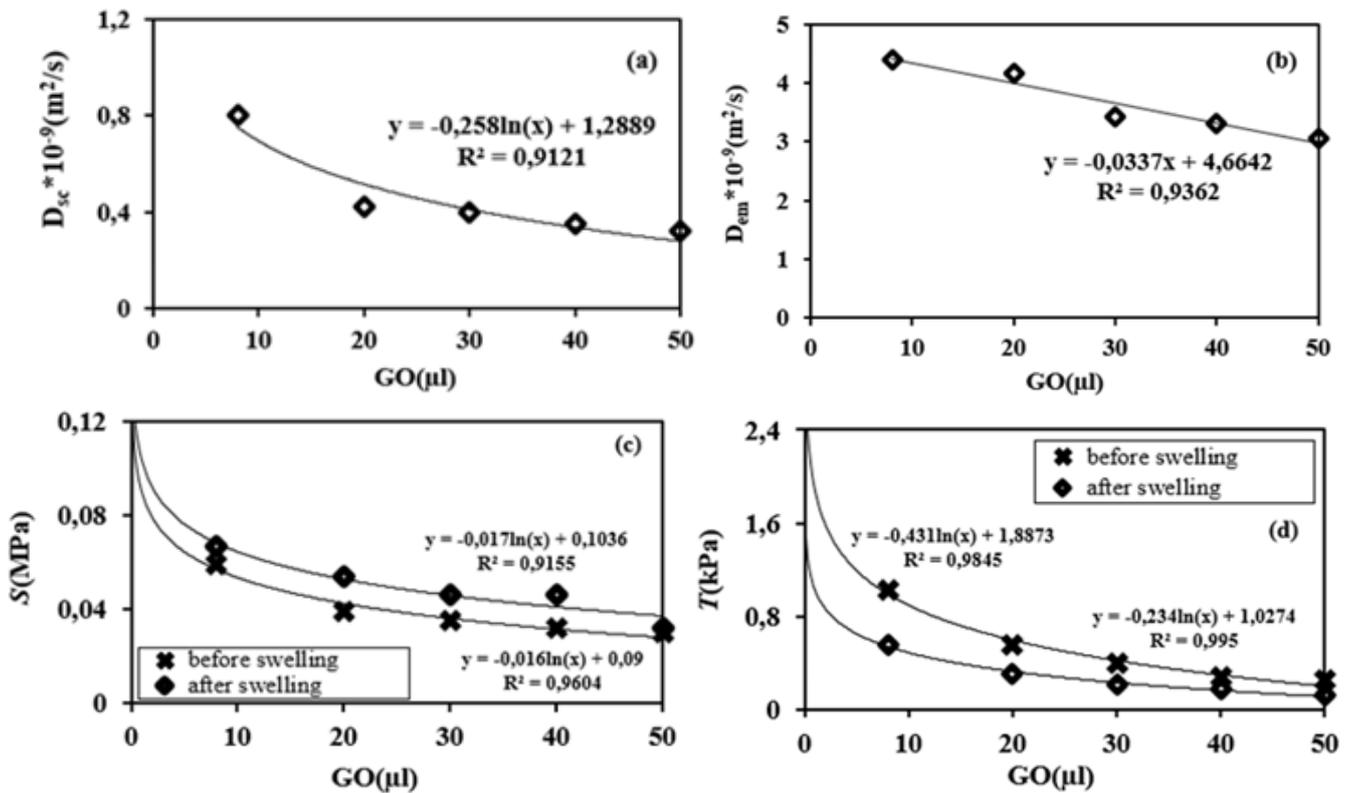
loading, respectively. The curves for compressive stress and strain before and after swelling for 40µl of the contents of GO at 30 °C are shown in Figure 5b. A stress and strain curve is drawn based on the following linear dependence with the values of load and displacement recorded in the experiment. The shear modulus,  $S$  is calculated according to the following equation (10):

$$S = \sigma(L_0/\Delta L) \quad (10)$$



**Figure 5(b):** Stress versus strain curves before and after swelling process for 40µl of GO content at 30 °C, respectively.

Where  $\Delta L$  is transverse displacement. The shear modulus,  $S$  is determined by the slope of the stress-strain curves within the linear elastic regime of less than 5% strain (see Figure 5b). The shear modulus as a function of different GO contents from mechanical measurements is shown in Figure 5. The shear modulus of GO - PAAm composites before and after swelling decrease with the increase of GO content above 8µl GO. It is also known that the swelling properties of composites mainly affect the shear modulus of the composites [1,14-16]. Here it can be seen that the composite has a lower  $G$ -value before swelling than after swelling, indicating higher toughness, i.e., high stiffness. A comparison of Figures 6a-6d shows that the diffusion coefficients  $D$  and the shear modulus  $S$  behave similarly as a function of the GO content, indicating that a higher GO content leads to tougher composite gels. In other words, the content of GO could act as a multifunctional crosslinker to form more compounds in the GO-PAAm composite and increase the crosslink density, leading to a decrease in swelling capacity. The toughness,  $T$  of the composite after swelling is found to be lower than the toughness after swelling between 8 and 50µl GO in Figure 6d [14]. It is obvious that toughness of composite gel with water must be less than the gel without water. It is also well known that the swelling properties of composite gels mainly affect the shear modulus and toughness of the composite gels. Because basically composite assembly based on intermolecular hydrogen bond or other non-covalent interactions was constructed in the presence of the GO and PAAm networks, which further affected swelling performances of the composites [16]. It was deduced that the GO content could act as a multifunctional cross-linker to form more junctions in GO-PAAm composite and increase the crosslink density, leading to the reduction of swelling capacity [2].



**Figure 6:** Diffusion coefficients,  $D_{sc}$  and  $D_{em}$  calculated from the data of (a) scattered light intensity, (b) the fluorescence intensity versus GO content in the composites for swelling process, (c) shear modulus and (d) toughness of GO-PAAM composites versus GO content before and after swelling process at 30 °C, respectively.

## Conclusion

The swelling and elasticity of graphene (GO) - polyacrylamide (PAAm) composites were investigated using fluorescence and compression techniques, respectively. The Fick's and Li Tanaka models were used to calculate the diffusion coefficients  $D_{sc}$  and  $D_{em}$ . The swelling of the composites was investigated as a function of GO. It was found that the diffusion coefficient and the cooperative diffusion coefficient decreased with increasing GO content. The shear modulus was also decreased before and after the swelling process from the critical value, which is at a content of  $8\mu\text{l}$  of GO. After reaching the highest shear modulus at  $8\mu\text{l}$  of GO, the shear modulus decreased with increasing GO content. Three contributions were identified, consisting of the degradation of physical cross-links, relaxation common to elastomers and swelling-induced relaxation, to produce the overall stress relaxation of GO -PAAm composites [1,14-16].

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