



Novel Adsorbent for Wastewater Treatment: Tailored Pore Size for Hazards from Aqueous Solution



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Abstract

Porous adsorption resin is one of the widely applied materials for removal of hazards from aqueous solution. The separation effect of resin is controlled by several interaction mechanisms, including sieving effect, electrostatic interactions and hydrogen bonds interaction. Resin pore size was reported to play an important role in the sieving effect of separation mechanism, which makes tailored pore size be considered as the main characteristic of next generation adsorbent. Here, we reviewed several widely used adsorption models and paid more attention to their potential values of calculating resin pore size for specialized target. We believe that this review is of certain significance and improvement of novel adsorption resins with tailored pore size. .

Keywords: Porous adsorption resins, Tailored pore size, Adsorption models; Waste water treatment

Opinion

Porous adsorption resins possess many special characteristics, such as various categories, high mechanical strength, porous availability, high surface area, and long life times, which make it widely used for separating targets and improve water quality [1-3]. As the title suggests, the important parameters of porous adsorption are pore structures and pore property. The IUPAC classification, in which pores are classified into macro- (>50nm), meso- (2-50nm), and micropores (<2nm) is based on the different mechanisms occurring in these pores during N₂ isothermal adsorption [4]. In order to gain a greater adsorption capacity and higher selectivity for toxic metallic species, chemical and physical modification is often undertaken to produce uniform adsorption resins by introducing selected functional groups into the matrix, which, in theory, modify the chemical composition of the surface of the adsorbents and hence improve their adsorption of target [5]. However, practical application by these modified resins is not much higher and their pore sizes result mainly from its single micro porous structure, which is unfavorable in adsorption application despite its greater surface area. Although many researchers are interested in enlarging the pore size of adsorption resins, research on the tailored pore size of adsorption onto resins lags severely. In several projects, the resins were modified to form more macro porous to increase adsorption capacity for wastewater treatment [6], but the various sizes of adsorbate were neglected. The chromium (VI) and arsenic (V) contamination in groundwater are major threat to human

health in many regions of the world, however the efficient pore size of resins for these two hazards are different, which were reported to be mesopores for chromium VI [7] and micropores for arsenic V [8]. Thus, the adsorption resins with tailored pore size are eager in the field of wastewater treatment. Before selecting optimal pore size for adsorbate, the interaction mechanism between resins and hazards need to be investigated. Sieving effect play an important role in separation and enrichment of molecule by adsorbent. In view of their particular application, this effect is basically controlled by pore physical structure, especially pore size and particle diameter. In addition, it is postulated that the pore size dictated the adsorption behavior with resins containing related larger pores following Langmuir model whereas those containing smaller pores following Freundlich model [9]. The classical adsorption kinetics model, Langmuir kinetics model (Equation 1), assumes the surface of adsorbate is energetically homogeneous [10,11].

$$\theta_A = \frac{V}{V_m} = \frac{K_{eq}^A p_A}{1 + K_{eq}^A p_A} \quad (1)$$

(p_A is adsorbate's partial pressure; V is the volume of adsorbate; θ_A is the fractional occupancy of the adsorption sites; V_m is the volume of the monolayer; K_{eq} is the associated equilibrium constant). By contrast, the Langmuir-Freundlich model (Equation 2) is another equation, which can't be solved analytically and considers the effect of surface heterogeneity [12-14]. However, the

rate constant of this model can be obtained by an approximation method.

$$\theta_A = \alpha_F p^{C_F} \tag{2}$$

(θ_A is the fractional occupancy of the adsorption sites; α_F and C_F are fitting parameters). These two adsorption behavior models usually lead different adsorption kinetics properties since the larger pore result in a faster adsorption equilibrium, correspondingly. Besides the primary mechanism of sieving effect, the separation and enrichment of adsorbate also rely on physical force, such as hydrogen bonds and electrostatic interactions. However, the interaction between resins and targets is mostly driven by different interaction with the order of sieving effect >> electrostatic interactions > hydrogen bonds. Moreover, the interaction of physical force is controlled by resins matrix and adsorbate structure, and tailoring resin pore size according to adsorbate do not affect the adsorption mechanism of physical force. Thus, the next generation of adsorbent for wastewater treatment is the tailored pore size for hazards from aqueous solution.

The model of calculating required pore size appears to be more important for the novel strategy of tailored resins. There is less attention on the potential practice-guiding impact of related model. Corroll and Berens suggested a three-parameter, two-compartment model (Equation 3) accounting for the influence of sphere diameter [15]. This monophasic model always gives a good fit of data in each case, however the adsorption is not considered as rapid, slow and even slower procedures, but only a global process instead.

$$\frac{q(t)}{q_0} = \frac{6}{\pi^2} \sum_{n=1}^{\infty} \frac{1}{n^2} [\phi_r \exp\left(\frac{-4n^2 \pi^2 D_r t}{a_r^2}\right) + (1 + \phi_r) \exp\left(\frac{-4n^2 \pi^2 D_s t}{a_s^2}\right)] \tag{3}$$

(ϕ_r is fast adsorption rate coefficient; a_r and a_s are the diameters of the spheres; D_r and D_s are diffusion coefficient). My project was performed in order to determine the adsorption profiles of adsorbate on resins [16,17]. According to the theory of the first-order, two-component four-parameter model, a new model [18] incorporating sphere size can be described by the following (Equation 4):

$$\frac{M_t}{M_0} = F_1 e^{-4 \times \frac{2^2 \pi^2 D_1 t}{r_1^2}} + F_2 e^{-4 \times \frac{2^2 \pi^2 D_2 t}{(r_1 + r_2)^2}} \tag{4}$$

(M_t is the solid-phase sorbate concentration at a given time, M_0 is the initial solid-phase adsorbate concentration, F_1 and F_2 are different compartments' fractions, D_r is the diffusion coefficient, and r_1 and r_2 are the diameters of the spheres, on which the different compartments of adsorption process are mainly carried out). This model provided a good fit of adsorption data, and a sphere size parameter was considered to be included to supply guiding of tailored pore size. In addition, further adsorption steps could be considered into the analysis process and a sphere-size model in which the adsorption process contains more compartments was proposed as (Equation 5).

$$\begin{aligned} \frac{M_t}{M_0} = & F_1 e^{-4 \times n^2 \pi^2 D_{r_1} t / r_1^2} + F_2 e^{-4 \times n^2 \pi^2 D_{r_2} t / (r_1 + r_2)^2} + \\ & F_3 e^{-4 \times n^2 \pi^2 D_{r_3} t / (r_1 + r_2 + r_3)^2} + \\ & \dots + F_n e^{-4 \times n^2 \pi^2 D_{r_n} t / (r_1 + r_2 + r_3 + \dots + r_n)^2} \end{aligned}$$

This model supplied parameters of sphere size, which could transformed to pore size according to BET results to reflects the effect of pore-size on adsorption kinetics process, and guides the selection or modification of porous adsorption resin for specialized target. Overall, the progress toward adsorption models with resin pore size is encouraging, and this is hope that further development of new calculating strategy of tailored pore size will help to bring forth better separation of targeted hazards from aqueous solution.

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