

# Assessment of Cooling Condensation and Adsorption Methods for Atmospheric Water Harvesting from Energy Point of View

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## Abstract

Different methods are developed to harvest water from the atmosphere. The most developed method for atmospheric water harvesting is cooling condensation method which is commercially available. There are also a number of research works on harvesting by using desiccant materials with some works at prototype and pilot scale. The energy consumption per collected water is of essential importance for water harvesting from the air. Here an assessment is made by simple calculations to analysis and compare these two methods.

## Introduction

Water scarcity is becoming a severe issue in different parts of the world. Although desalination is an effective way for water shortage, but the main problem is difficulty to supply remote regions far away from water resources. Atmospheric water harvesting (AWH) is an alternative solution for local water supply [1]. Different techniques are developed for AWH. Among them cooling condensation is most developed and commercially available technique. There is a lot of works on adsorption AWH in which vapor can be concentrated by using desiccants that adsorb the vapor from the air and can later be recovered in a thermal-driven step [2].

In cooling condensation technique to have one cubic meter of water at 4 °C, about 698KWh energy is theoretically required [3]. Lower relative humidity of the air makes lower dew point temperature that increase energy consumption as significant amount of energy is spent for cooling of the air. From 500 to 7000KWh/m<sup>3</sup> energy consumption is reported depending on the air humidity, temperature and the atmospheric water generator (AWG) design [4].

The problem is harvesting atmospheric water in an energy efficient way. Since harvesting air humidity by direct cooling may wastes a large portion of the energy on cooling the air [5], concentrating the water vapor can reduce this sensible heat load [6]. Kim et al. [7] analysis indicates that the adsorption-based approach is superior to refrigeration systems. Adsorption-based AWH performs better than traditional, refrigeration-based dewing systems particularly in arid, low humidity climates [8].

It is state that the cooling condensation works well at humid regions [9]. The purpose of the present work is assessing the energy consumption in cooling condensation and adsorption methods for atmospheric water harvesting by simple calculations based on the sensible heat and enthalpy to indicate the energy efficient regions for each method.

## Results and Discussions

Heat capacities of air and average heat capacity of common adsorbents are known and so sensible heat can be easily calculated. Here the average heat capacity on common MOFs

is used for calculations.  $C_{p,air} = 1.006 \text{ KJ/Kg.k}$  (at  $0 \text{ }^\circ\text{C}$ - $25 \text{ }^\circ\text{C}$ ) and  $C_{p,MOFs \text{ Average}} = 0.904 \text{ KJ/Kg.k}$  [10]. Average enthalpy of adsorption for common MOFs is  $2860 \text{ KJ/kg KJ/Kgwater}$  [11] and enthalpy of water evaporation is equal to  $2261 \text{ KJ/Kg}_{water}$ . The air temperature is assumed to be  $25 \text{ }^\circ\text{C}$  and desorption temperature is assumed  $70 \text{ }^\circ\text{C}$ . For both methods the sensible heat changes at different conditions but the enthalpy of evaporation or adsorption is fixed. The basis of calculations is  $1 \text{ kg}$  harvested water. Total energy is the sum of sensible heat and the heat of adsorption. For adsorption method from  $10 \text{ wt}\%$  to  $100 \text{ wt}\%$  adsorption is considered from low humidity to higher humidity. The results for adsorption AWH are presented in Table 1.

**Table 1:** Adsorption AWH. Sensible heat of adsorption =  $m_{MOF} * C_{p,MOF} * (70 \text{ }^\circ\text{C} - 25 \text{ }^\circ\text{C})$ .

Adsorption capacity gr-w/g-ads	Energy KJ/Kg	Harvested Water kg/Cycle
0.1	$40.68/0.1 \text{ kg (sensible)} + 2860$ (enthalpy) = $3266.8/\text{kg}$	1
0.2	$40.68/0.2 + 2860 = 3063.4/\text{kg}$	1
0.4	2961.7	1
0.6	2927.8	1
0.8	2910.85	1
1.0	2900.68	1

For cooling condensation from  $30\% \text{ RH}$  to  $100\% \text{ RH}$  is considered and shown in Table 2. Total energy is the sum of sensible heat and the heat of evaporation. At  $20\%$  relative humidity (RH), the dew point at  $25 \text{ }^\circ\text{C}$  is  $-1.2 \text{ }^\circ\text{C}$  and the cooling condensation cannot work.

**Table 2:** Cooling condensation AWH. Sensible heat =  $m_{air} * C_{p,air} * (25 \text{ }^\circ\text{C} - \text{dew } ^\circ\text{C})$ .

RH (t=25 °C)	Dew point	Sensible + enthalpy KJ	Harvested Water
30	5.2	$3521 + 2444.44 = 5965.44$	1
40	9.8	$2027.24 + 2444.44 = 4471.68$	1
50	13.4	$1238.83 + 2444.44 = 3684.27$	1
60	16.4	$764.66 + 2444.44 = 3209.10$	1
70	19	$457.27 + 2444.44 = 2901.71$	1
80	21.2	$253.41 + 2444.44 = 2697.85$	1
90	23.2	$106.70 + 2444.44 = 2551.14$	1
100	25	$0 + 2444.44 = 2444.44$	1

As it can be seen in comparison with Table 1, for RH higher than  $70\%$  the energy consumption of cooling condensation is lower than adsorption AWG. But in region below  $50\%$  down to  $30\%$  the consumption increases dramatically. And below  $30\%$  the cooling condensation cannot work because of under zero dew point and the problem of freezing. Therefore, at dry region below  $30\%$  the cooling condensation essentially is unable to work and adsorption AWG can perform well. As RH decreases the sensible heat for cooling condensation AWH is considerably increased while this sensible heat is much lower for adsorption AWH.

## The real conditions

The above calculations include the sensible heat and heat of adsorption but there is heat and mass transfer inside the bed and porous adsorbent which make more energy consumption and need optimum design to reduce the total energy consumption. For the cooling condensation there is also heat transfer inside the mass of the passing air through condenser and also some design considerations are necessary to increase the performance of the system to condense maximum possible water from the air. In addition, there is pump and compressor with less than  $100\%$  efficiency that increase the energy consumption.

Beside these general problems about  $628 \text{ kWh/m}^3$  is just needed for condensation of water but the reports by manufacturers show even lower consumption while prototype experimental data shows much higher consumptions [4]. The lower consumption reported by manufacturers has a few reasons. First the condenser for cooling the refrigeration fluid is air cooled and uses no external energy for cooling. The 2nd is a kind of intelligent control to decide the AWG works or not. When the RH is lower than a specified threshold the system does not work. The system may work at nighttime in humid region where the air is close to its dew point and use less sensible energy to be cool down. It is possible that the temperature at some point equals the dew point and with no consumption the condensation happen in the condenser (evaporator). The reports may be yearly average, and the outcome is consumption less than the enthalpy of evaporation as the minimum consumption. And finally, the optimum design of the AWH unit reduces the energy consumption while a simple experimental prototype has the lack of optimum design and intelligent control system.

We have to notice that in sophisticated design a hydrophobic surface becomes easily wet and nucleation of water vapor occurs and the condensation at  $100\%$  humidity and even lower humidity close to saturation can happen and less energy is required for condensation than what is calculated at Table 2 for  $100\% \text{ RH}$  or close to it.

## Conclusion

The results clearly show that at high humidity the cooling condensation is favorable. At RH more than  $70\%$  the energy consumption of cooling condensation begins to be lower than that of adsorption AWH. Less than  $50\% \text{ RH}$ , adsorption AWH shows to be more energy efficient and less than  $30\% \text{ RH}$  because of under zero dew point the cooling condensation is unable to work while the adsorption AWH performs well. For adsorption AWH there is difference between single cycle and multicycle regimes. In a single cycle which definitely use direct solar power the adsorption capacity is important as daily harvested water is equal to water-uptake/cycle. But in a multicycle system the sensible heat is less than  $20\%$  of total energy consumption (Table 1) and adsorption capacity is less effective (minor parameter) in the energy consumption per harvested water. Even at humid regions if it is intended to have solar driven AWH the solution is adsorption AWH

as the cooling condensation cannot use the direct solar energy and needed external power.

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